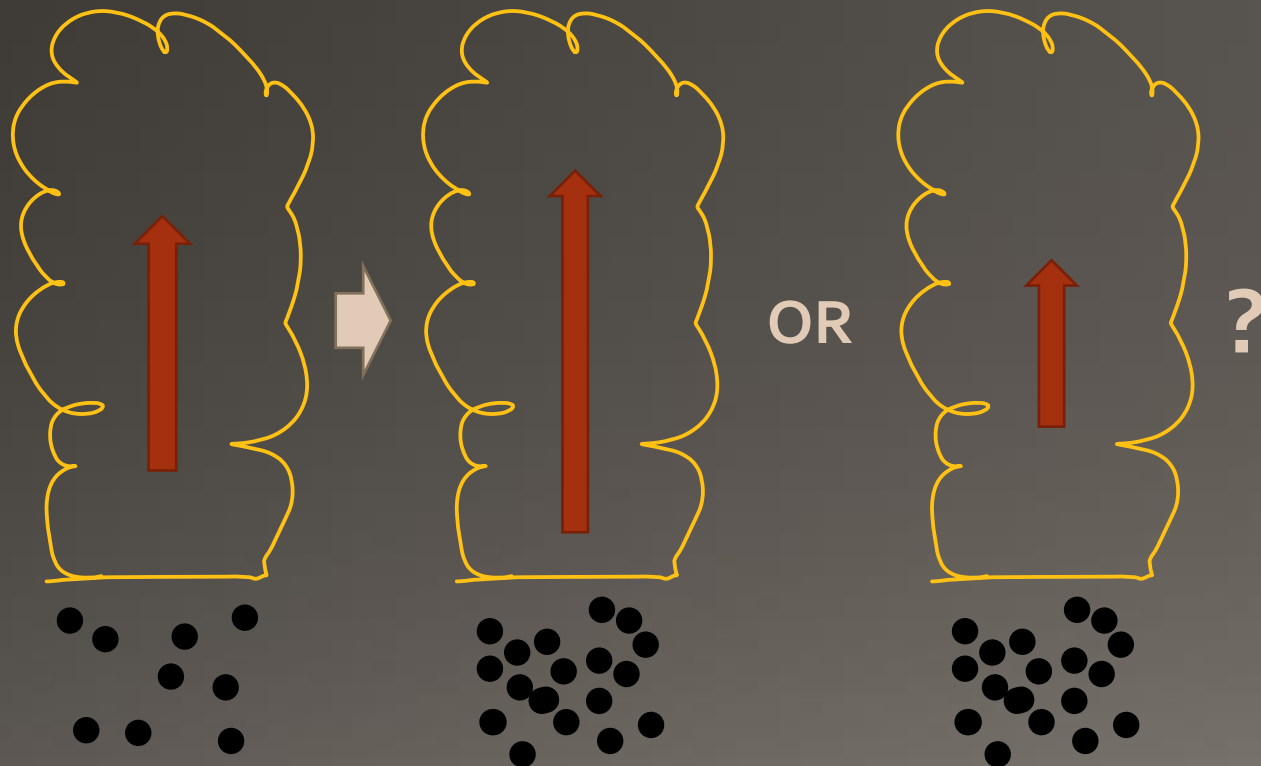


# Invigoration or Enervation of Convective Clouds by Aerosols?



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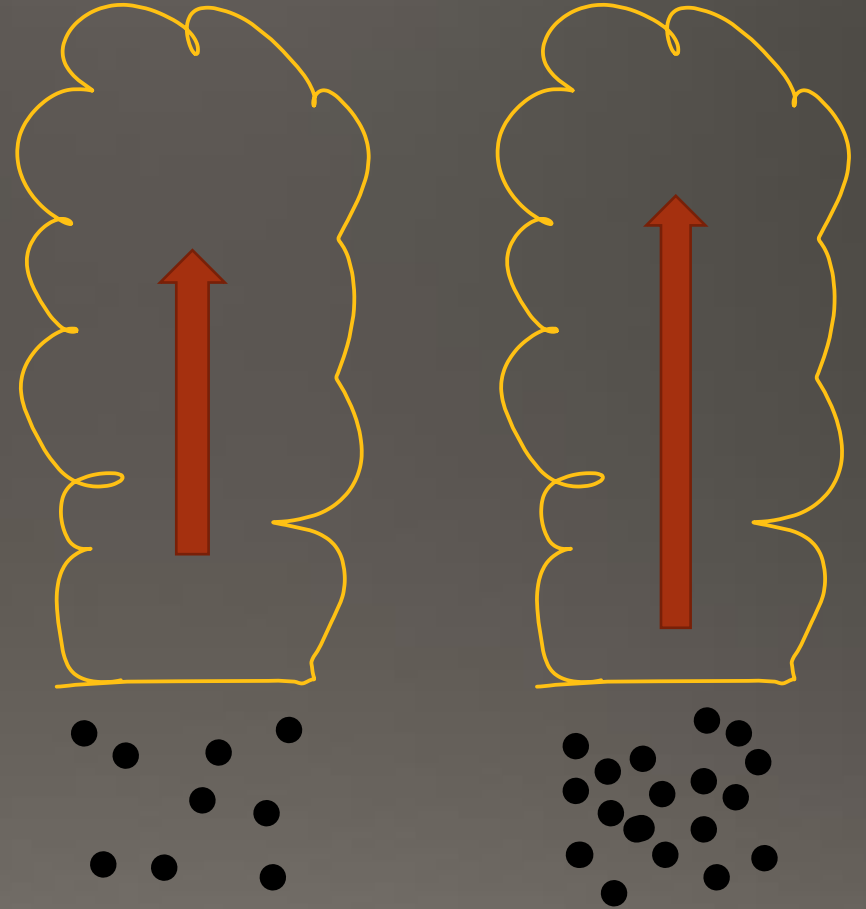
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**Invigoration or Enervation of Convective Clouds by  
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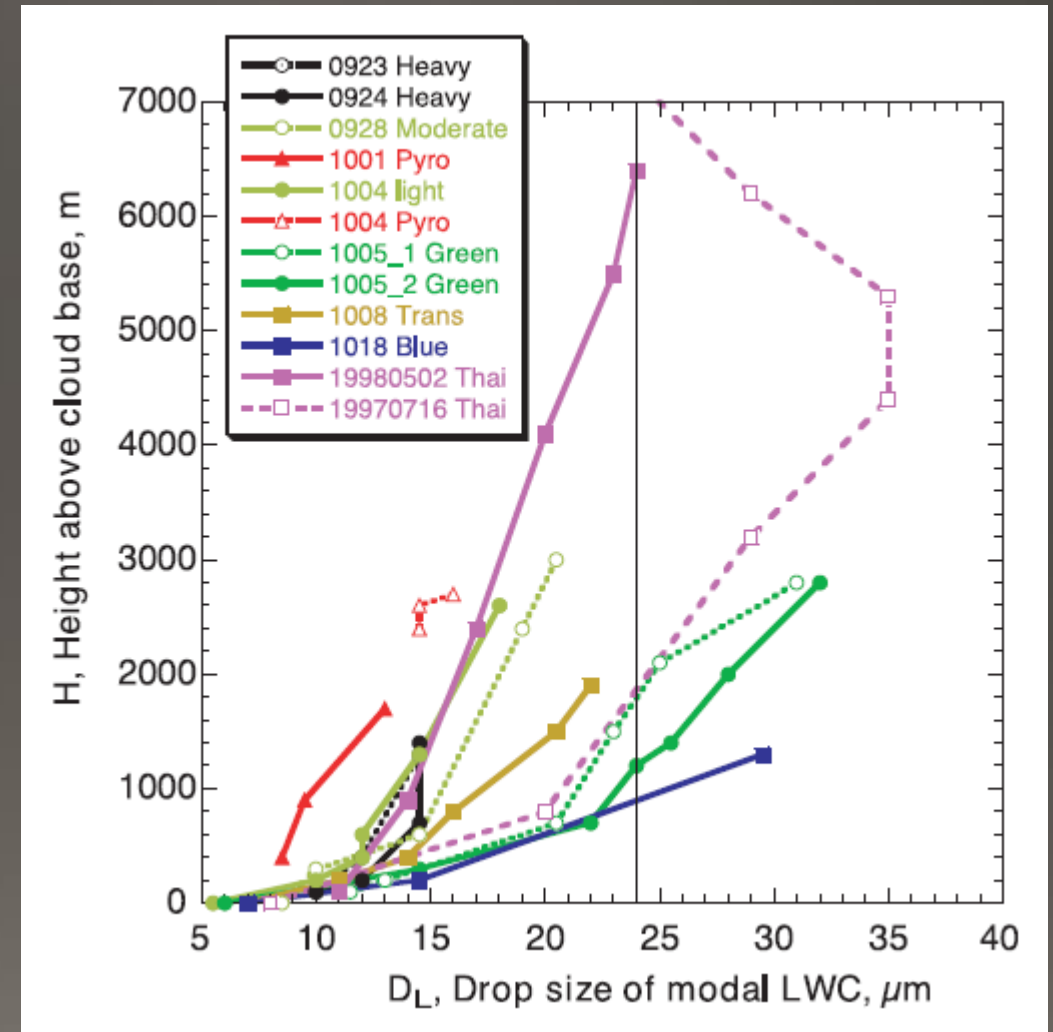
# Aerosol-Induced Invigoration

- “**Invigoration**” here refers to the idea that convective storms that ingest higher aerosol particle concentrations will develop **stronger updrafts**
- Lots of proxies for updraft strength, here we use CAPE.



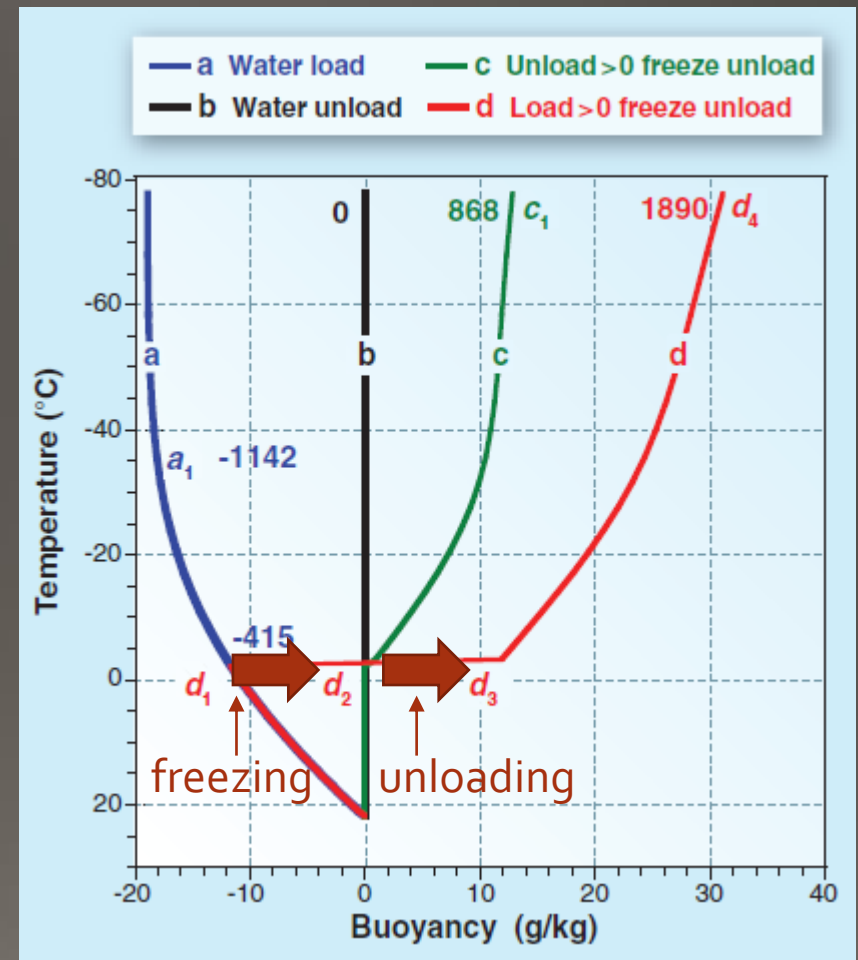
# “Cold-phase” invigoration hypothesis

- The common explanation:
- More cloud droplets suppresses rain formation and precipitation
  - As a result, more liquid water is lofted above the freezing level
  - The extra liquid freezes and releases latent heat, increasing buoyancy of the updraft
  - The updraft strengthens
- Prominently described by Rosenfeld et al. (2008)



# “Cold-phase” invigoration hypothesis

- This common explanation misses a key point from Rosenfeld et al. (2008)
- “Freezing all the cloud water would warm the air and add thermal buoyancy by an amount that would almost exactly balance the condensate load (d<sub>2</sub>). When the ice hydrometeors precipitate from a parcel, it becomes more positively buoyant because of its reduced weight (d<sub>3</sub>).”



# “Warm-phase” invigoration hypothesis

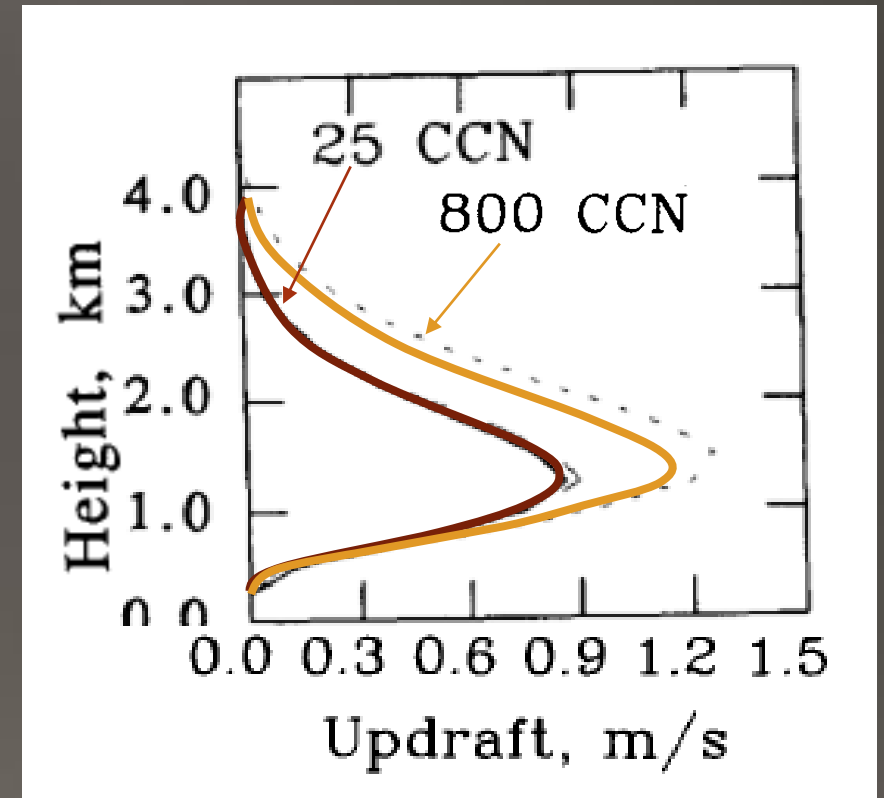
- Smaller, more numerous droplets grow by condensation faster.

- $condensation \propto N\bar{D}$

→ More latent heat is released and increases the buoyancy of the updraft.

→ Also, supersaturation is reduced.

→ The updraft strengthens.



Kogan and Martin 1994

# GOAL

To theoretically assess the magnitude of the cold-phase and warm-phase invigoration hypotheses

# Use Parcel Theory to Evaluate the Hypotheses

- Updraft speed is related to CAPE:  $CAPE = \frac{1}{2} w^2$
- CAPE depends on the parcel properties and the environment:

$$CAPE = \int_{p_{LFC}}^{p_{EL}} R_d \frac{T_{\rho,ENV} - T_{\rho}}{p} dp$$

- Conveniently, **DIFFERENCES in CAPE** between two parcels A and B in the same environment are independent of the environment:

$$\Delta CAPE = \int_{p_{LFC}}^{p_{EL}} R_d \frac{T_{\rho,A}(p) - T_{\rho,B}(p)}{p} dp$$

To calculate  $\Delta CAPE$ , we need to specify  $T_{\rho}(p) \rightarrow$  need an equation for  $\frac{dT}{dp}$  that accounts for freezing, condensate loading, and supersaturation

# A New Lapse Rate Equation

- A new equation for  $dT/dp$  was derived that accounts for the three necessary processes of supersaturation, freezing, and condensate loading

$$\frac{dT}{dp} = \frac{\frac{TR_0}{p_0} + \frac{L_{F1}r_1}{p_0} \left(1 - \frac{d \ln S}{d \ln p}\right)}{c_p + L_{32}r_F \frac{d\xi}{dT} + L_{F1}r_1 \frac{p}{p_0} \frac{d \ln p^{21}}{dT}}$$

Supersaturation change with pressure

Condensate loading impacts these two terms

Freezing term;  $\xi$  is frozen fraction



# A New Lapse Rate Equation

- The equation is numerically integrated to arrive at profiles of temperature, water vapor, liquid, and ice
- To solve, several assumptions must be made:
  1. Condensate loading as a function of pressure  $r_F(p)$
  2. Frozen fraction as a function of temperature  $\frac{d\xi}{dT}$
  3. Supersaturation as a function of pressure  $\frac{d\ln S}{d\ln p}$
- These assumptions can be varied in ways that are consistent with aerosol effects

# Unrealistic Condensate Loading and Freezing Assumptions

	Clean	Polluted
Condensate loading assumption	No condensate loading	Condensate loading until freezing, then complete unloading
Freezing assumption	100% ice starting at $-4^{\circ}\text{C}$	100% ice starting at $-4^{\circ}\text{C}$

Condensate unloading may not be complete – partial unloading may occur

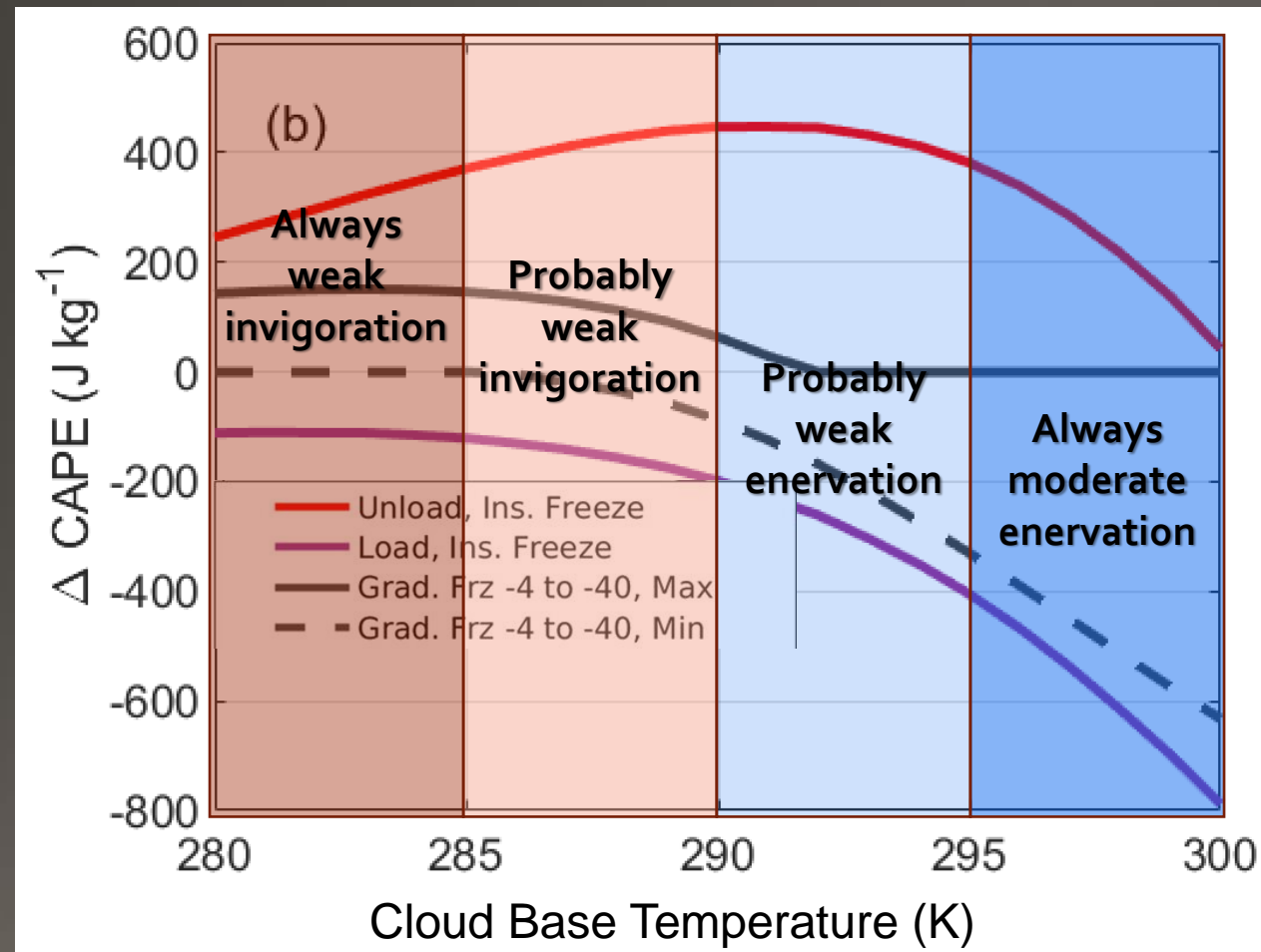
Condensate unloading is not instantaneous – it may occur gradually instead

Freezing is not instantaneous at  $-4^{\circ}\text{C}$  – it is gradual down to  $-40^{\circ}\text{C}$

# More Realistic Condensate Loading and Freezing Assumptions

	Clean	Polluted
Condensate loading assumption	<p>No loading</p> <p>The unloaded fraction and loading threshold are both varied.</p>	
Freezing assumption	<p>Linearly freeze between -4 and -40 °C</p>	<p>Linearly freeze between -4 and -40 °C</p>

# More Realistic Assumptions

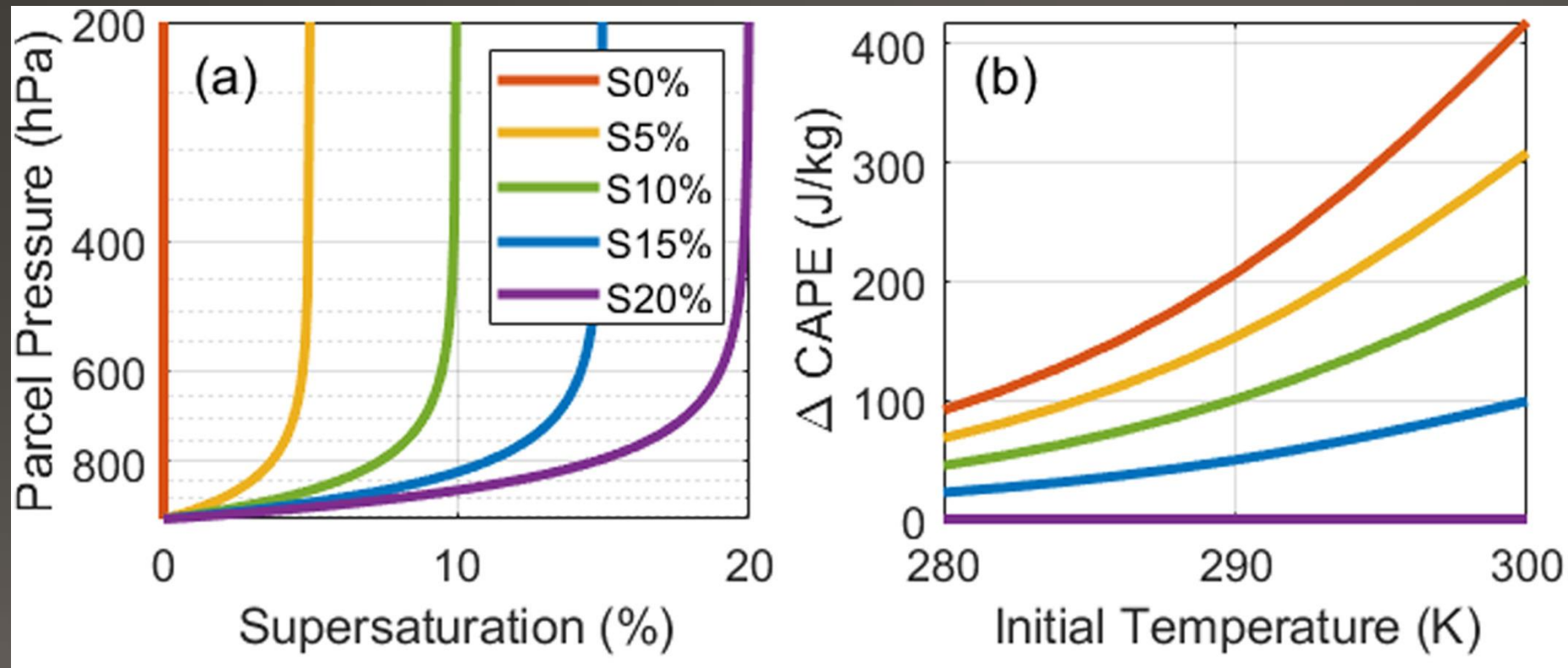


# Warm-Phase Invigoration

	Clean	Polluted
Condensate loading assumption	No condensate unloading	No condensate unloading
Freezing assumption	Linearly freeze between -4 and -40 °C	Linearly freeze between -4 and -40 °C
Supersaturation assumption	Equilibrium SS of 20%	Equilibrium SS < 20%

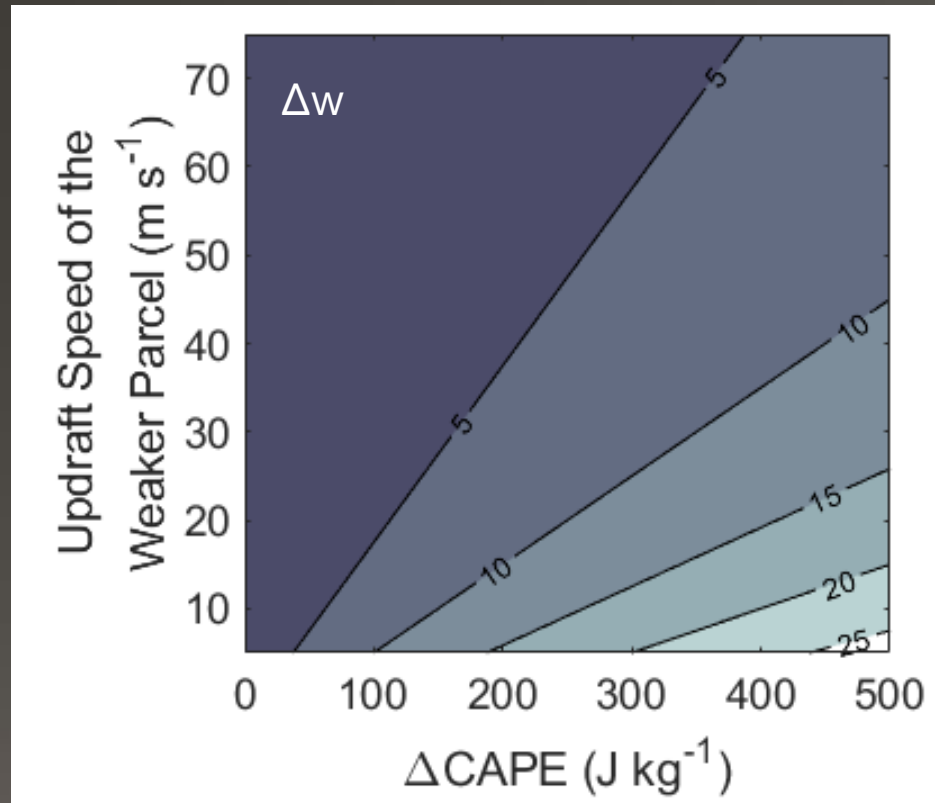
# Warm-Phase Invigoration

- $\Delta$ CAPE of up to  $\sim 100$  J/kg for every 5% change in supersaturation
- Can't say from this study what a realistic change in SS is.



# CAPE and Updrafts

- $CAPE = \frac{1}{2} w^2$  (we know this equation overestimates  $w$ )



- Naturally weak storms are most susceptible to invigoration/enervation
- For  $\Delta CAPE \sim 400 \text{ J/kg}$ , maximum  $\Delta w \sim 10 \text{ m/s}$  assuming that values are too large by a factor of 2
- May be hard to observe

# Take-Home Points

- Cold-phase invigoration relies on condensate unloading, not just freezing
  - For storms with bases  $> 290\text{K}$ , aerosol-induced changes to cold-phase processes may result in enervation, not invigoration
- Warm-phase invigoration is plausible but requires very large changes in supersaturation to be important
- Aerosol-induced changes in updraft speed are likely  $\sim 10$  m/s or less in naturally weak storms and  $\sim 5$  m/s or less in naturally strong storms